

Investigation of microstructure of irradiated multilayer $\text{ZrN}/\text{Si}_3\text{N}_4$ thin coatings revealed by X-ray diffraction techniques

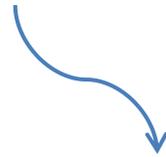
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Why nitride-based thin films?

Various applications as protective coatings

- microelectronics,
- optics,
- **nuclear applications,**
- ...



Properties suitable for nuclear applications:

- high melting point
- high hardness
- stability under elevated temperatures
- wear and corrosion resistance
- good thermal conductivity
- good mechanical properties



Radiation tolerant coating materials



estimation of the effects of radiation damage

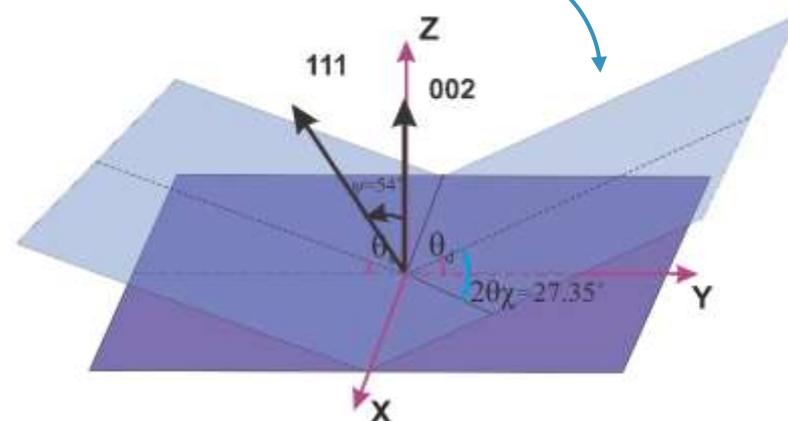
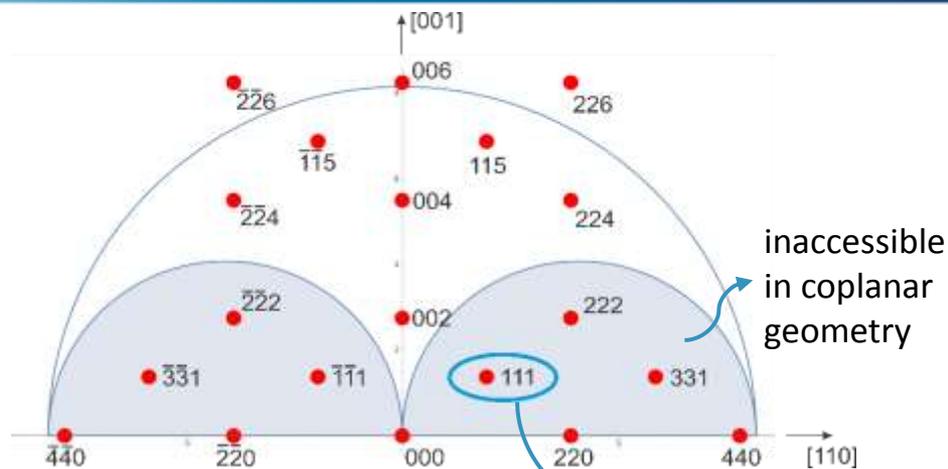


modification of microstructure under the irradiation process.



Techniques to characterize thin films:

- Reciprocal space mapping (RSM),
- Pole figures
- Grazing incidence XRD (GIXRD)
- $\theta/2\theta$ scanning (coplanar geometry)
- **Non-coplanar geometry** 



Why non-coplanar measurement geometry?

- access to a larger number of Bragg reflections
- no tilt of the sample (important for high-temperature measurements)
- no rotation of the sample
- insufficient resolution: a set of two orthogonal Soller slits are used
- coplanar GIXRD does not permit to cover the whole range of ψ angles (because of 2θ limits)

Purposes of the research:

- evaluate microstructural parameters using theoretical analysis of XRD data, measured in non-coplanar geometry
- estimate if the microstructure undergoes changes under irradiation
- compare the results of XRD and HRTEM

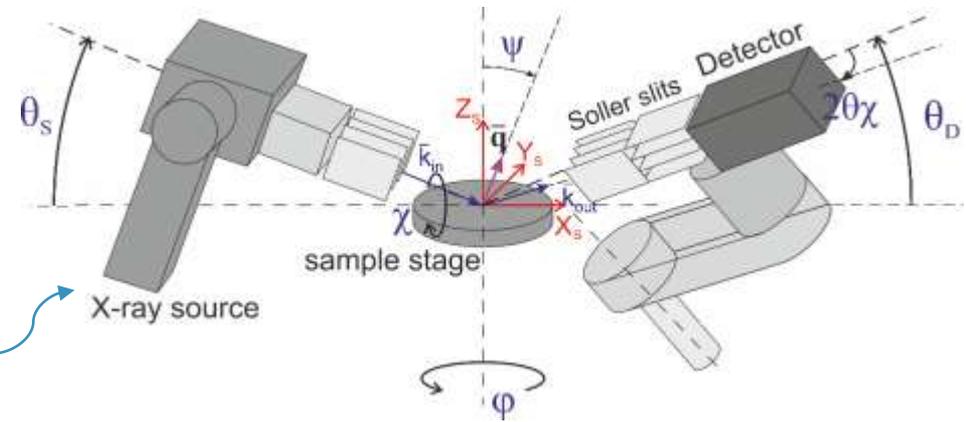
Investigation techniques:

- X-ray diffraction (XRD)
- High-resolution transmission electron microscopy (HRTEM)
- Theoretical analysis

Diffractometer setup:

- Cu K α radiation ($\lambda = 0.154056$ nm)
- parallel beam geometry
- set of two orthogonal receiving Soller slits

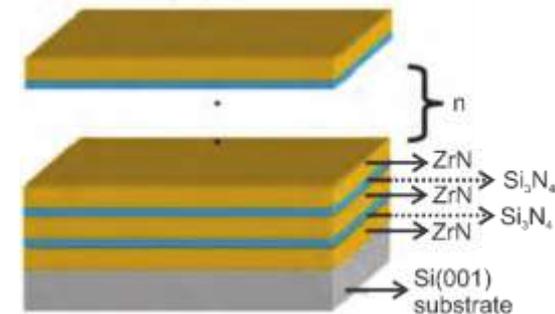
Non-coplanar measurement configuration



Samples:

- crystalline/amorphous multilayers
ZrN/Si₃N₄
- single crystal Si (001) substrate
- total thickness of each multilayer:
300 nm

- **ML-1:** 5 nm/5 nm
 - **ML-2:** 10 nm/5 nm
 - **ML-3:** 5 nm/2 nm
 - **ML-4:** 10 nm/0.4 nm
- unirr. + irr. unirr.



Irradiation conditions:

- 30 keV He⁺ ions
- integral dose: $5 \cdot 10^{16} \text{ cm}^{-2}$

Pole figures: $I = I(\psi, \varphi)$



Texture (preferred orientation)



best conditions (ψ angles) for
observing other reflections



best conditions for scanning mode:
varying θ_s, θ_D ($\theta_s = \theta_D$),
fixed $2\theta \neq 0$



XRD measurements

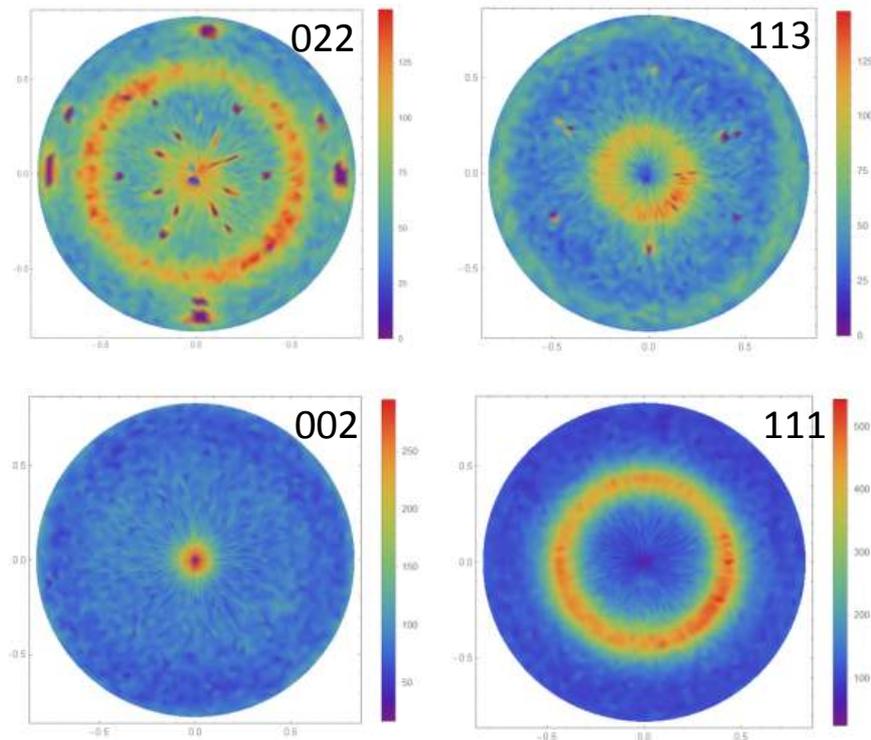
Pole figures: $I = I(\psi, \varphi)$

Texture (preferred orientation)

best conditions (ψ angles) for observing other reflections

best conditions for scanning mode:
varying θ_s, θ_D ($\theta_s = \theta_D$),
fixed $2\theta_{\chi} \neq 0$

XRD measurements



Axial symmetry

[001] direction – orthogonal to the sample surface

Pole figures: $I = I(\psi, \varphi)$



Texture (preferred orientation)



best conditions (ψ angles) for observing other reflections



best conditions for scanning mode:
varying θ_s, θ_D ($\theta_s = \theta_D$),
fixed $2\theta_{\chi} \neq 0$



XRD measurements

$$\cos \psi (\theta_s, 2\theta_x) = \frac{2 \sin \theta_s \cos^2 \theta_x}{\sqrt{2 - 2 \cos(2\theta_s) \cos(2\theta_x)}}$$

$$\cos(2\theta) = \cos(\theta_s + \theta_D) \cos(2\theta_x)$$



Optimal instrumental angles for measuring scans

reflection	111	002	022	113	222	004
ψ , deg	54.00	0	45.00	24.00	54.00	0
$2\theta_{\chi}$, deg	27.35	0	39.79	26.50	58.36	0
$2\theta_s$, deg	20.00	39.00	45.00	62.00	53.00	84.00
2θ , deg	33.95	39.41	56.96	67.99	71.46	84.80

Pole figures: $I = I(\psi, \varphi)$



Texture (preferred orientation)



best conditions (ψ angles) for observing other reflections

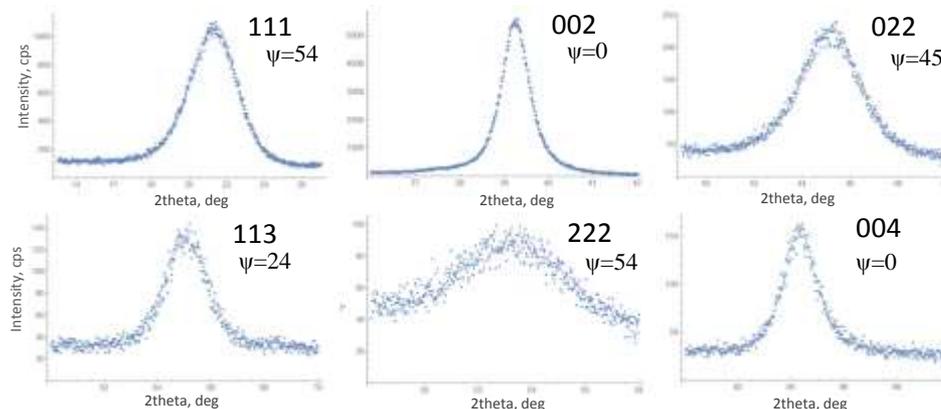


best conditions for scanning mode:
varying θ_s, θ_D ($\theta_s = \theta_D$),
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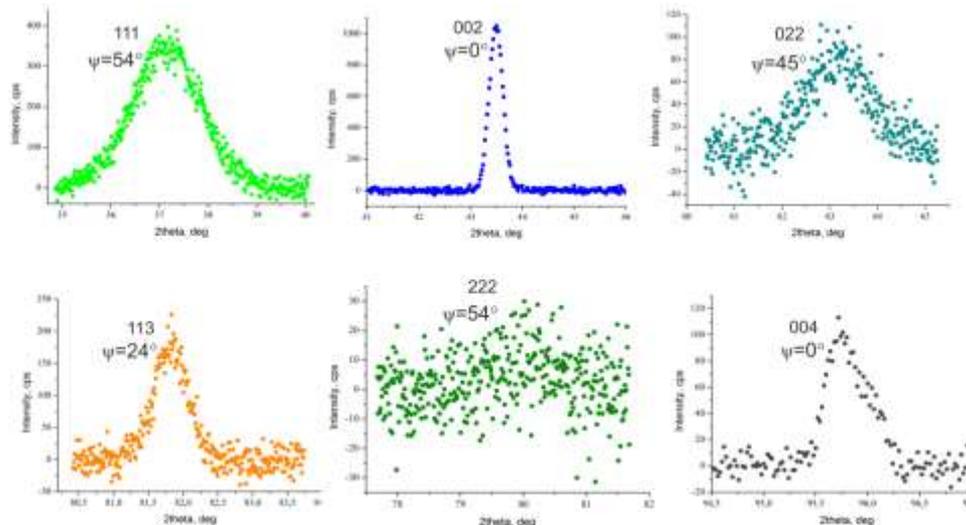


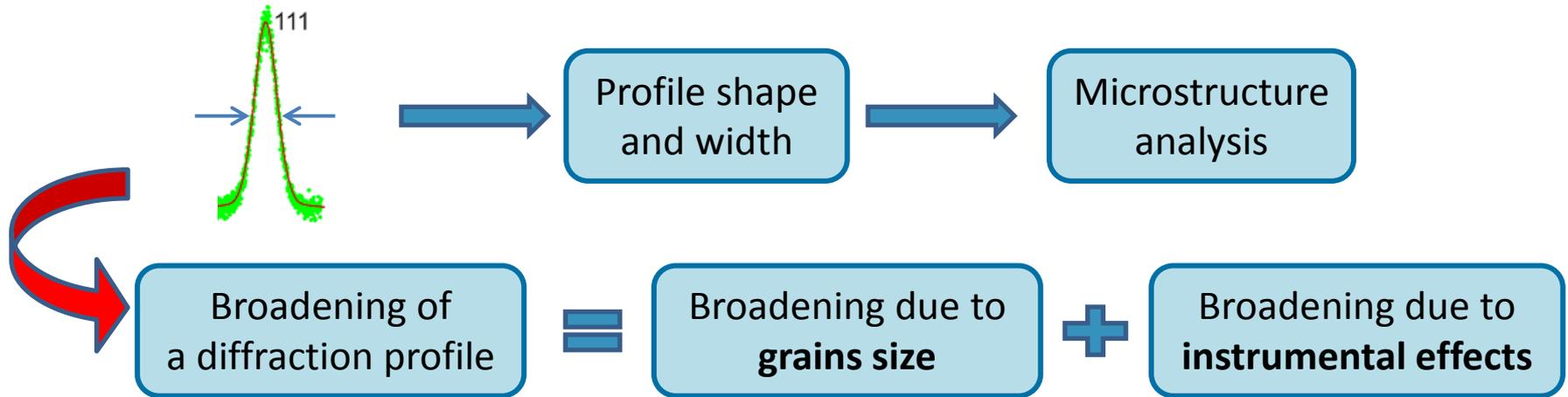
XRD measurements

XRD profiles: polycrystalline ZrN layers



Instrumental function: LaB6 powder





Theoretical curve:

$$I_{theor} = \sum_{hkl} I_{max}^{hkl} I_{size}^{hkl} (2\theta - 2\theta_0^{hkl}) * I_{instr}^{hkl} (2\theta - 2\theta_0^{hkl})$$

Faster performance

Calculations in Fourier space

$$A(L) = A_{size}^{hkl}(L) A_{instr}^{hkl}(L)$$

Grain sizes distribution: **Gauss distribution function**

$$f(x) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left[-\frac{(x - m_{hkl})^2}{2\sigma^2}\right]$$

Shape of grains?

spherical
(most simple and obvious)



ODS steels (structural material for nuclear applications)

Proved by HRTEM

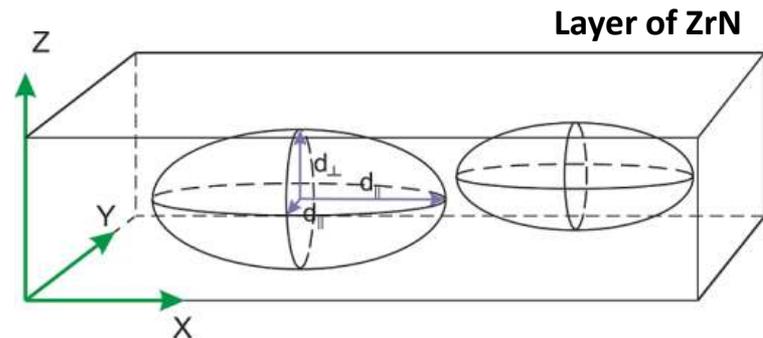
parallelepiped



ellipsoidal



best consistence between measured and theoretical profiles



When applying an ellipsoidal grain shape model, the **size distribution** function becomes **anisotropic**, with the appearing dependence of the reflection intensity on the hkl .

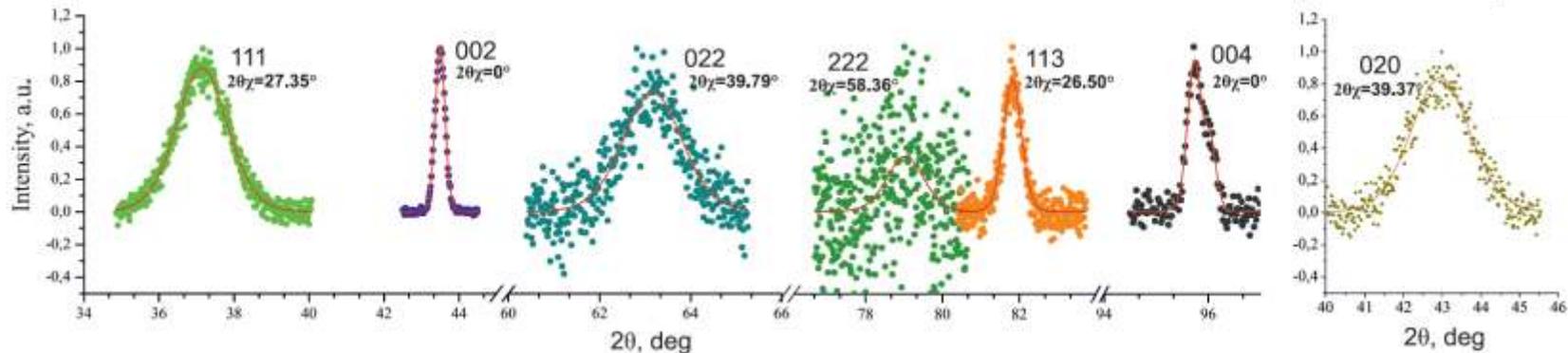
$$m_{hkl} = \frac{m}{\sqrt{1 + \left(\frac{1}{e^2} - 1\right) \cos^2 \psi}},$$

$$\cos \psi = \frac{l}{\sqrt{h^2 + k^2 + l^2}}, \quad e = \frac{c}{a}$$

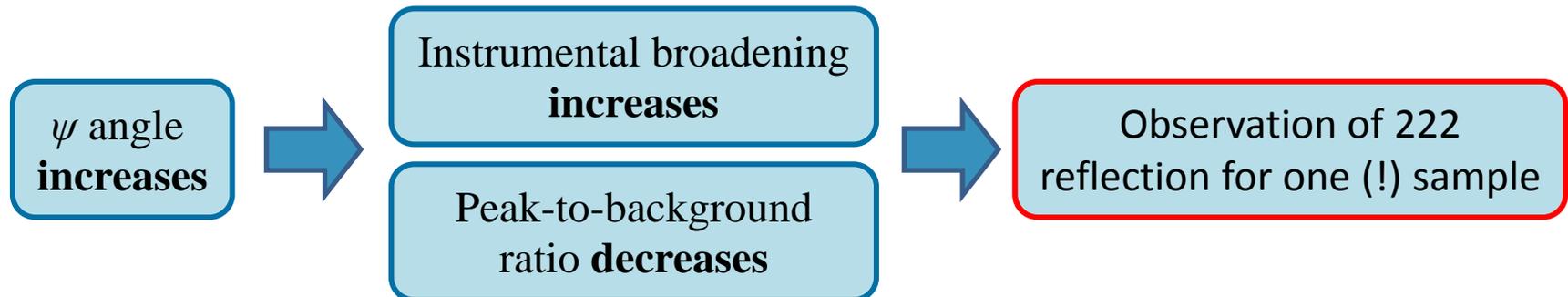
Assuming ellipsoidal grains, the hkl -dependent **size broadening** is given by

$$A_{size}^{hkl}(L) = \frac{1}{6} (2m^3 + 6m\sigma^2 - 3\sigma^2|L|) + \frac{1}{6} \exp \left[-\frac{(m - |L|)^2}{2\sigma^2} \right] \sqrt{\frac{2}{\pi}} \sigma (-2m^2 - 4\sigma^2 + |L|(m + |L|)) - \frac{1}{6} \{2m^3 + 6m\sigma^2 - 3\sigma^2|L| - 3m^2|L| + |L|^3\} \operatorname{Erfc} \left[\frac{|L| - m}{\sqrt{2}\sigma} \right]$$

For accounting the **instrumental effects**, a set of LaB₆ profiles were measured and used as instrumental profiles I_{instr}^{hkl}

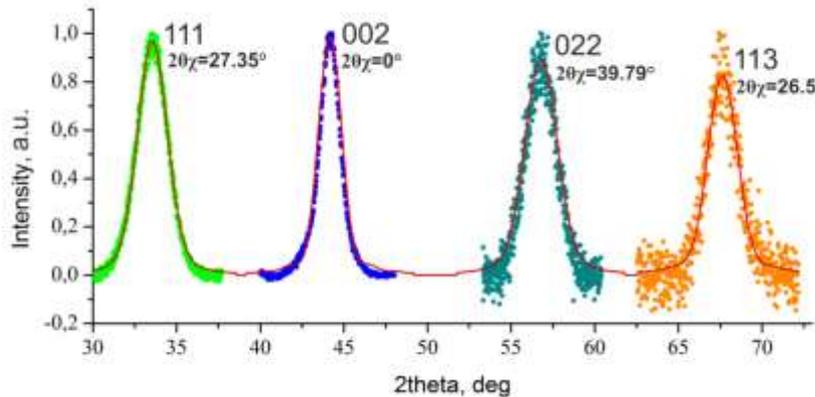


The instrumental function plays a crucial role in the non-coplanar measurements.

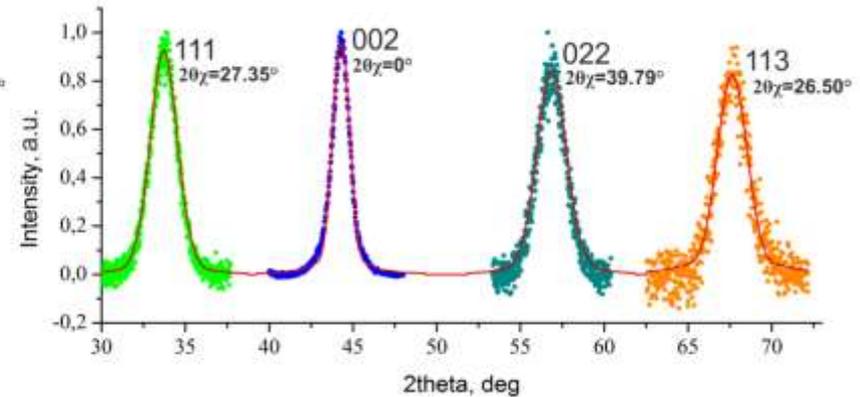


The reflections, obtained under different ψ angles, are combined into a single scan for the simultaneous fitting with a theoretically simulated curve.

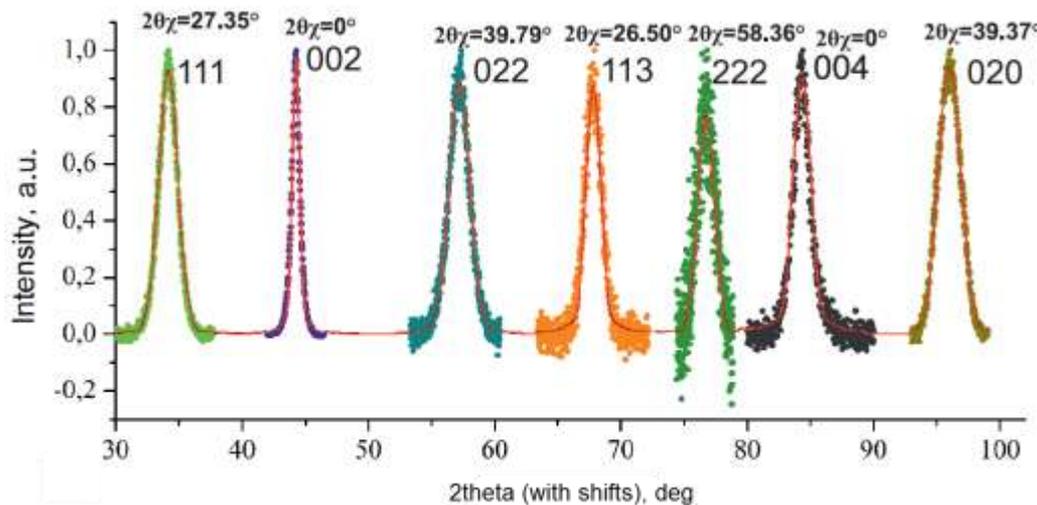
Four unirradiated and three irradiated by the He⁺ ions samples were evaluated to estimate the modification of sample microstructure under the irradiation process.



Unirradiated ML-3 sample

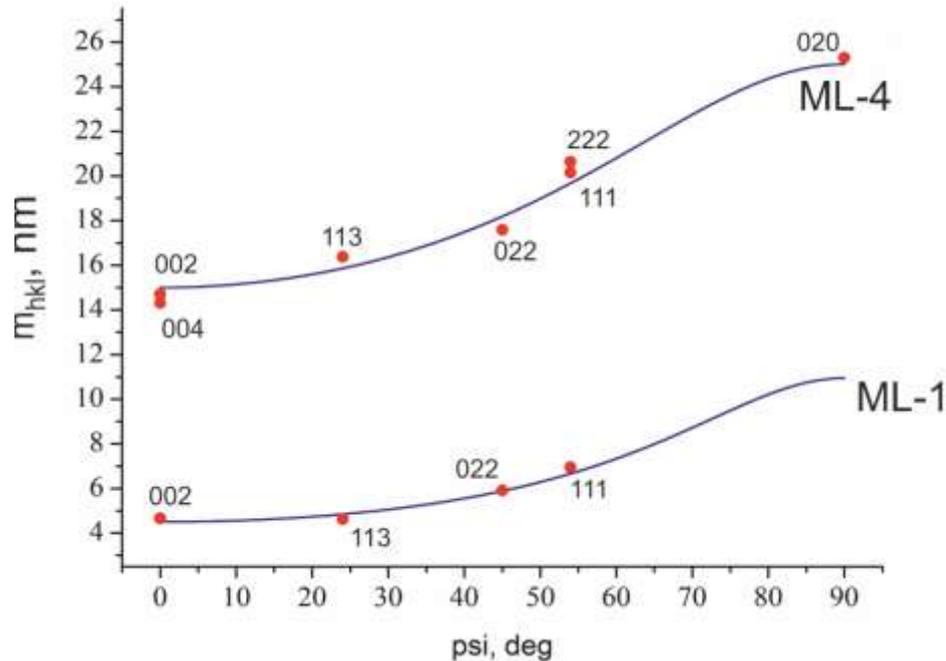


Irradiated ML-3 sample



Unirradiated ML-4 sample

The measured **direction-dependent broadening** was in agreement with the assumed shape.



Theoretical curves
(assuming ellipsoidal grains)

$$m_{hkl} = \frac{m}{\sqrt{1 + \left(\frac{1}{\epsilon^2} - 1\right) \cos^2 \psi}},$$

$$\cos \psi = \frac{l}{\sqrt{h^2 + k^2 + l^2}}, \quad \epsilon = \frac{c}{a}$$

Experimental points
(from single profiles)

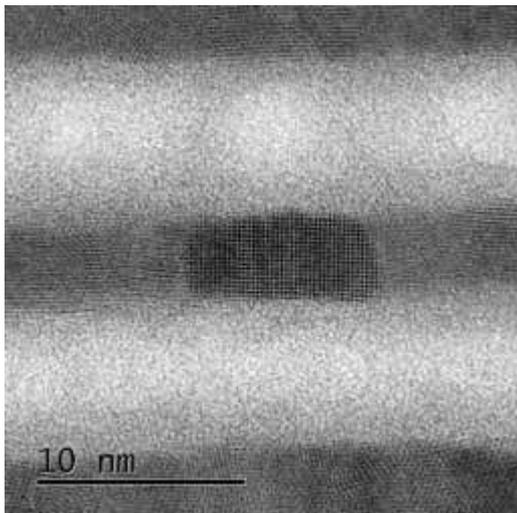
- The microstructural parameters obtained from the fitting of the whole scan and those obtained solely for 020 reflection ($\psi \approx 90^\circ$) are in a very good agreement, which confirms the correctness of the size estimation in the direction parallel to the sample surface.
- For the sample ML-4, the multiple reflections 002 and 004, 111 and 222 are observed, and m_{hkl} for these reflections are close each to other, which confirms the absence of the line broadening caused by the defects.

Preparation of the experiment:

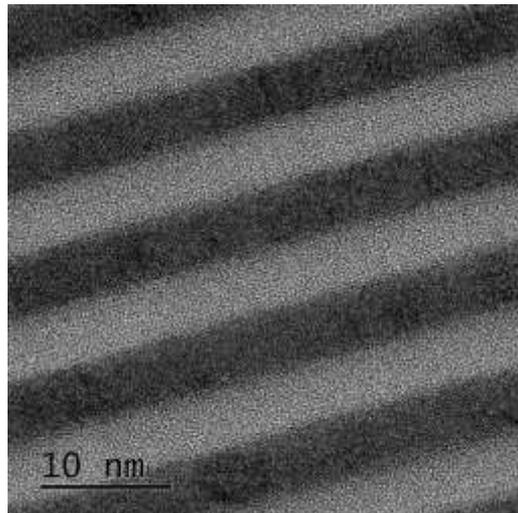
- specimens were prepared using **FEI Helios Nanolab 650** focused ion beam
- initial milling – 30 keV Ga ions
- final thinning – 5 keV
- polishing - 2keV and 500 eV
- analysis - **JEOL JEM 2100** LaB6 transmission electron microscope (200 kV)



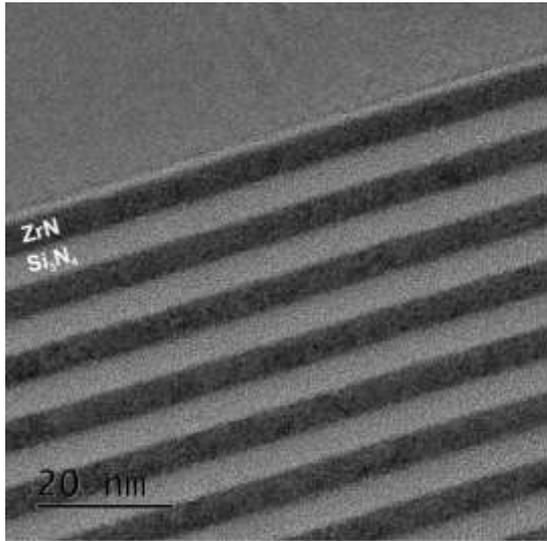
Image of grains



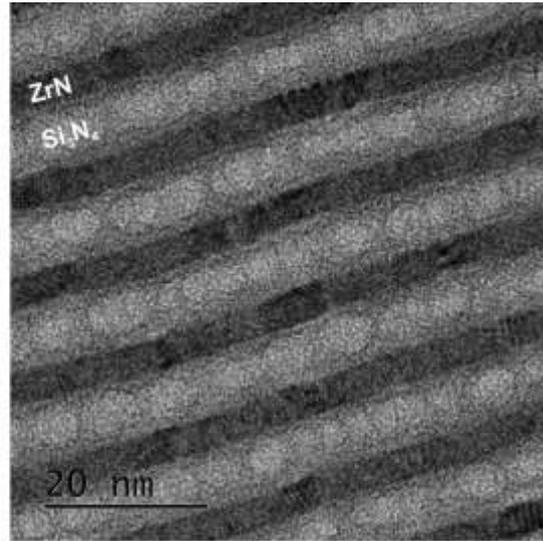
High-resolution TEM



Unirradiated ML-3



Irradiated by He+ ML-3



After the irradiation:

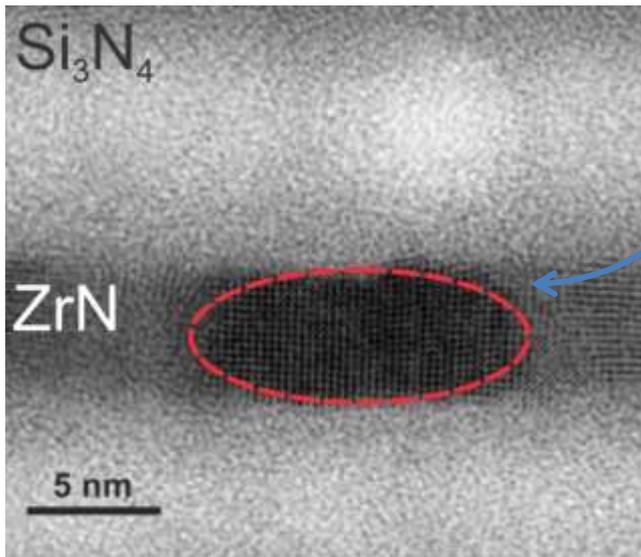
- the thickness of the ZrN is almost the same,
- the thickness of the amorphous layers undergoes a significant increase.

Possible explanation:

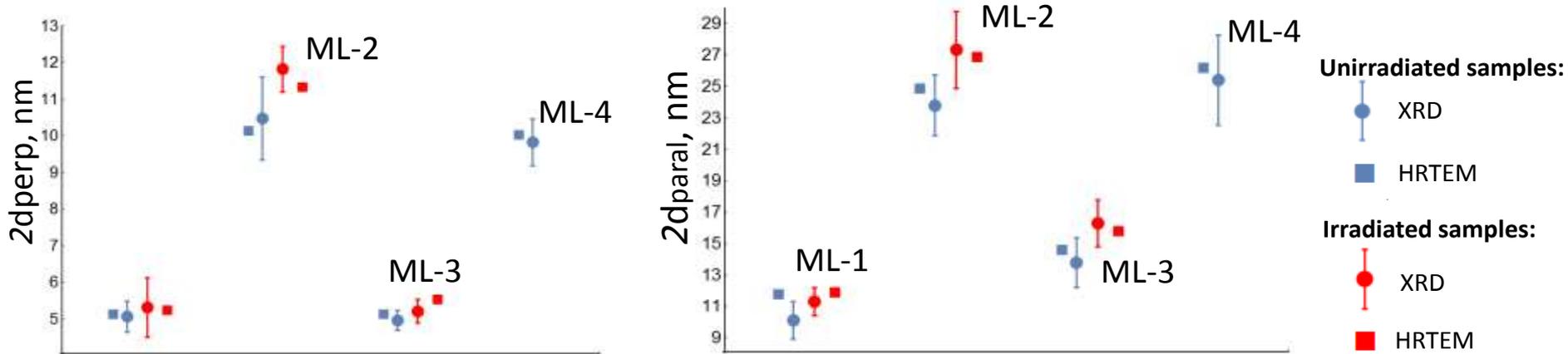
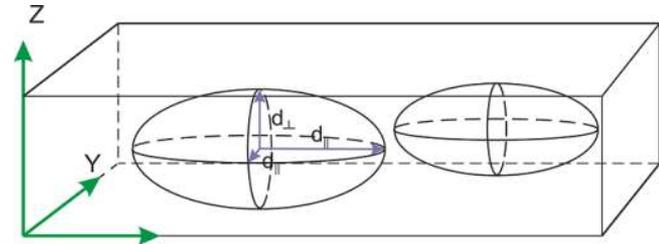
bubble formation during the irradiation



deformation of the crystalline/amorphous interfaces due to the appearance of residual stresses



As a result of the fitting procedure, the **average grain size** in the **directions parallel** and **normal** to the sample surface have been evaluated.



- A good consistence between the XRD and HRTEM results for **unirradiated samples** confirms the validity of the used theoretical model.
- A good agreement between the results of XRD and HRTEM for **irradiated samples** means that after irradiation **no significant amount of defects appeared**.
- **Grains size** in the samples after irradiation **does not differ significantly** from that before the irradiation.

- ✓ The microstructural parameters of ZrN/Si₃N₄ multilayer thin coatings have been evaluated using X-ray diffraction technique in non-coplanar geometry.
- ✓ The non-coplanar X-ray diffraction geometry gives an access to a larger number of Bragg reflections comparing to the case of a coplanar configuration.
- ✓ The technique enables to perform a comprehensive and reliable analysis of the samples possessing the anisotropy of physical properties.
- ✓ Using the theoretical model for ellipsoidal grains, the sizes of grains in parallel and normal to the sample surface directions were calculated.
- ✓ The results obtained from XRD measurements are in a good agreement with those evaluated from HRTEM and STEM.
- ✓ Comparing the results of XRD analysis and HRTEM for unirradiated and irradiated samples, the microstructure of investigated samples is proved to do not undergo a significant change under the irradiation process.
- ✓ The proposed approach can also be extended to include other sources of diffraction line broadening which occurs in different materials.

Thank you for your attention!

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